Geometric Dependencies of Mean ExB Shearing Rate in Negative Triangularity Tokamaks

[Singh, Diamond, Nelson NF 2023]

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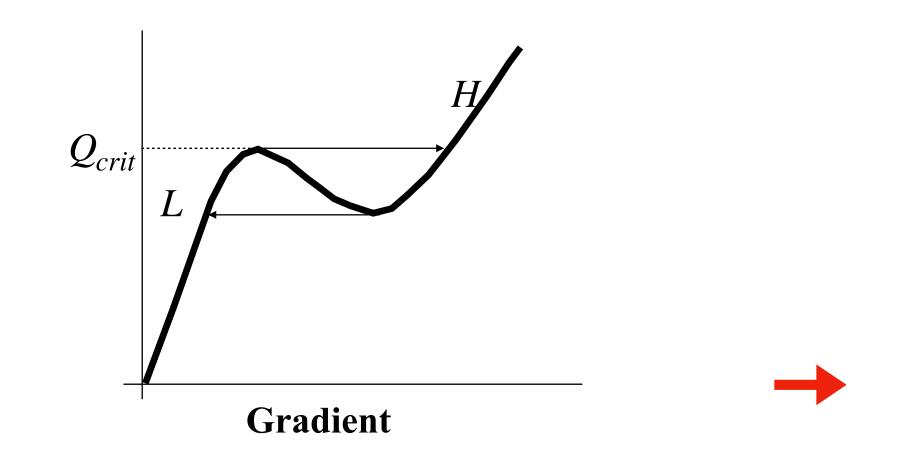
65th APS DPP Conference Oct 30 - 03, 2023 Denver, Colorado

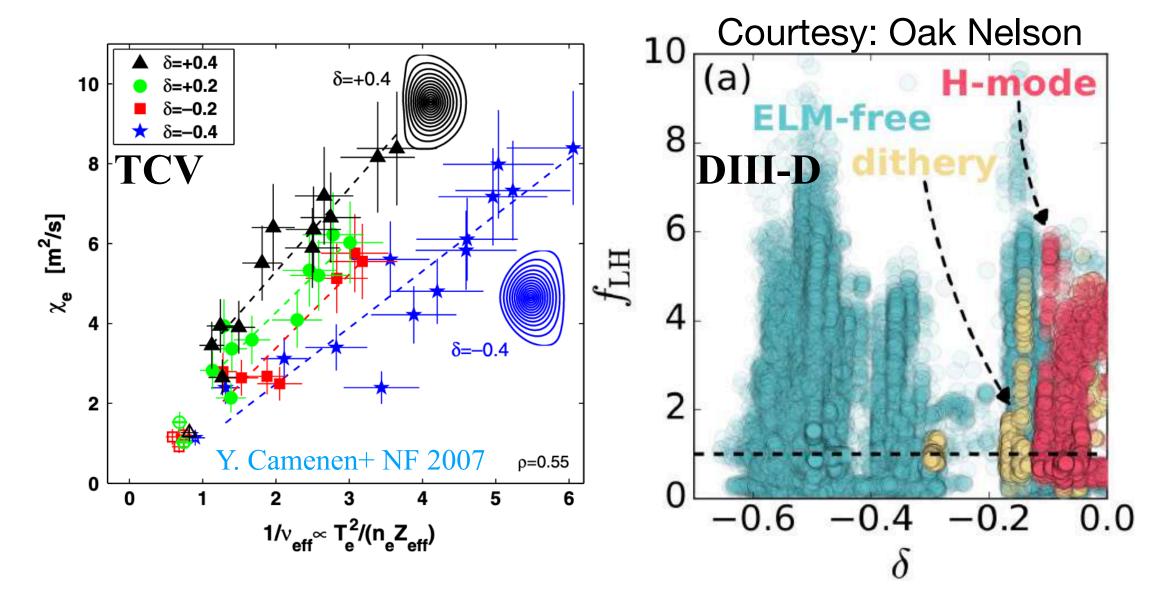
Acknowledgements: T. S. Hahm, L. Schmitz, K. Thome and "Neg. Triang. Cabalists" DIII-D.

U.S. Department of Energy Award Number DE-FG02-04ER54738.

Effect of triangularity on confinement, fluctuations, and L-H transition

- TCV: Energy confinement time doubled, fluctuations reduced when $\delta \to -\delta$
- DIII-D: No H-mode transition for $\delta < \delta_{crit} \sim -0.18$
 - $P_{L \to H}$ diverges for $\delta < \delta_{crit}$.
 - loss of access to 2nd stability region of $n = \infty$ ideal MHD ballooning modes for $\delta < \delta_{crit}$ [Saarelma+ PPCF 2021, Nelson+ NF 2022].



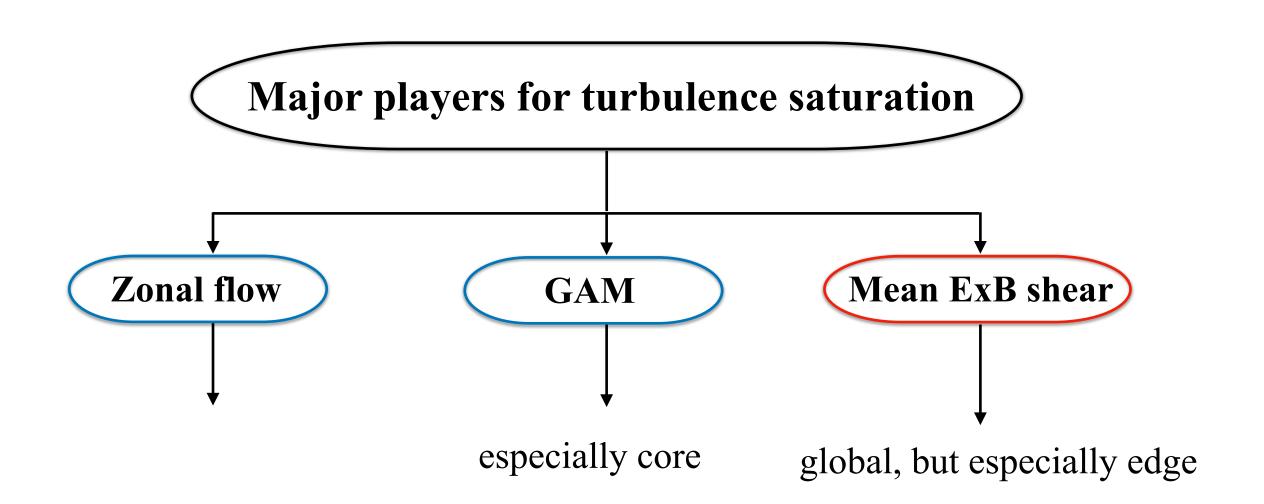


- Is H mode operation always in 2nd stability region?
 - Magnetic separatrix + finite edge current → coalescence of 1st and 2nd stable region. [Bishop NF 1986]
 - H-mode persisted even after loss of 2nd stability. [L Lao + NF 1999, J R Ferron+ NF 2000]
- What happens to the E_r^\prime induced transport bifurcation picture of L-H transition in NT?

Role of mean ExB shear in NT pedestal formation?

How to reconcile confinement improvement in NT L-mode with diverging $P_{th,L\to H}$ for $\delta < \delta_{crit}$?

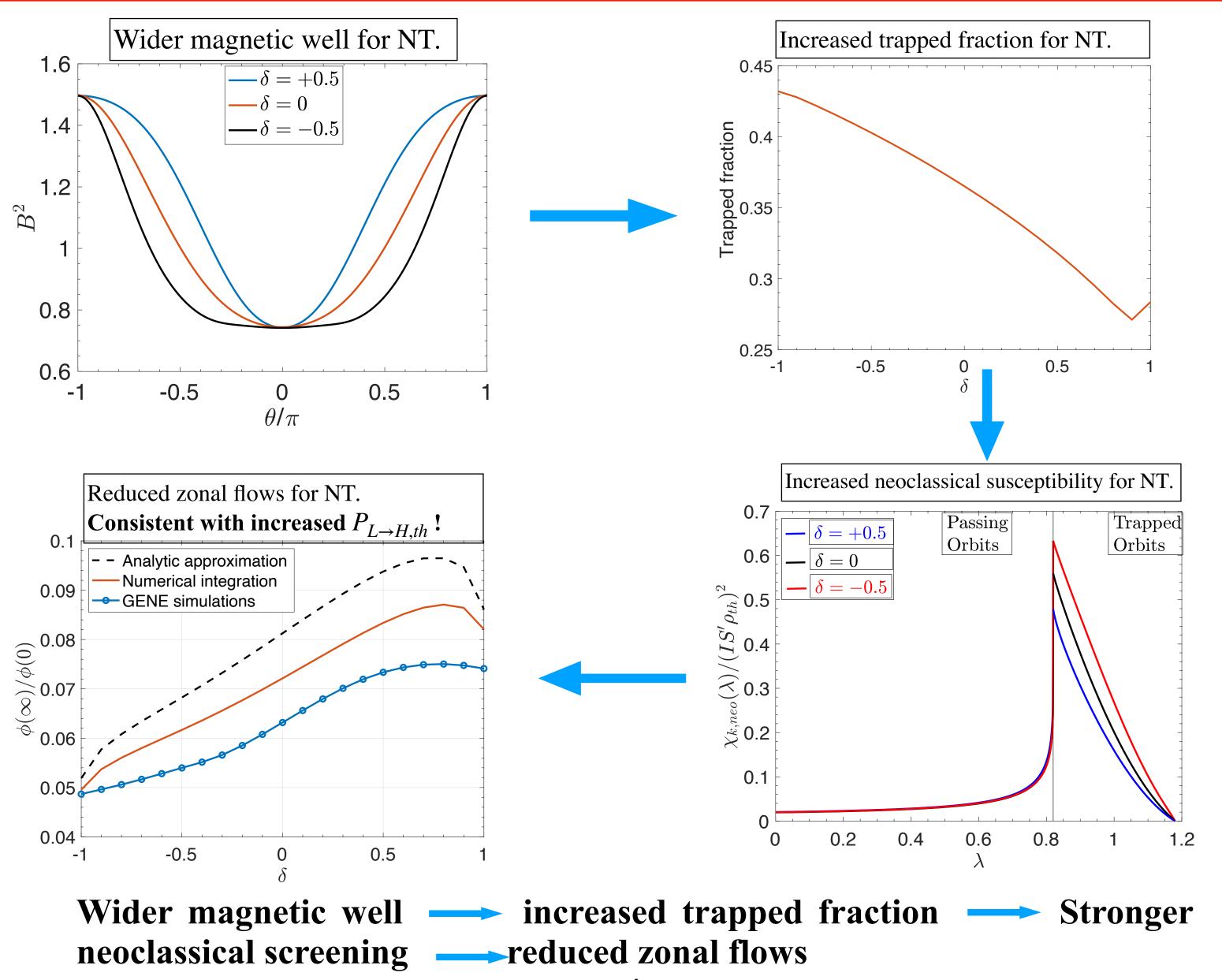
- Need think beyond linear stabilization of zoo of modes(TEM/ITG,...)!
- Understanding flux surface shaping effects on turbulence saturation mechanism is important.



• Interplay of NT configuration with secondary modes feedback and shearing?

Zonal flows are reduced in NT

[Singh and Diamond NF 2022]



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Geometry dependence of mean ExB shearing rate ω_E

ExB shearing rate in general axisymmetric toroidal geometry obtained from a 2-point correlation calculation:

[Hahm & Burrell PoP 1995]

$$\omega_E = \left(\frac{\Delta \psi_0}{\Delta \zeta}\right) \frac{\partial^2}{\partial \psi^2} \Phi_0(\psi),$$

 ψ := poloidal flux ζ := toroidal angle

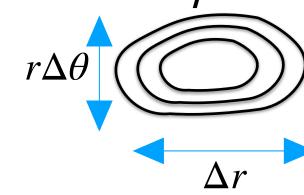
 Φ_0 := Mean electrostatic potential

 $\Delta \psi_0$:=Turbulence correlation length in ψ

 $\Delta \zeta$:=Turbulence correlation in toroidal angle ζ

- $\frac{\partial^2}{\partial w^2} \Phi_0(\psi)$ is set by the radial force balance of ions as usual!
- $\Delta \psi$ is related to turbulence radial correlation length Δr : $\Delta \psi = \Delta r \frac{\partial \psi}{\partial r}$, where ψ' is obtained from the definition of global safety factor q: $\psi' = \frac{I(\psi)}{2\pi a(\psi)} \oint d\theta \frac{\mathcal{J}}{R^2}$
- $\Delta \zeta$ is related to poloidal correlation angle $\Delta \zeta = \nu \Delta \theta$, where the local safety factor $\nu = \frac{I \mathcal{F}}{R^2 \psi'}$

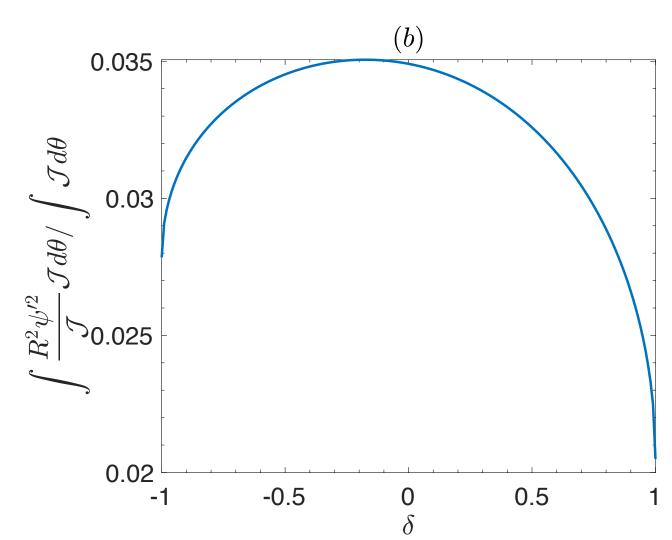
. Thus,
$$\omega_E=\frac{\Delta r}{\Delta \theta} R^2 \psi'^2 \frac{\partial^2}{\partial \psi^2} \Phi_0(\psi),$$
 Geometry dependent factor



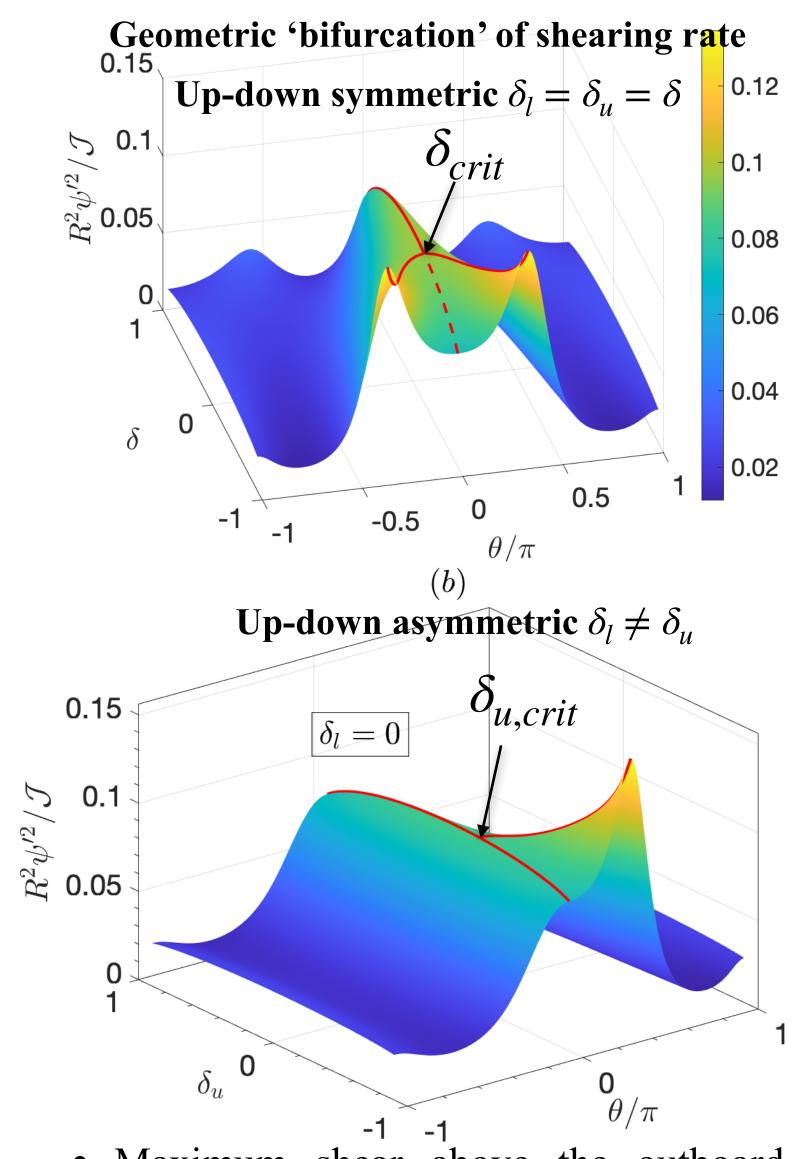
Calculated for Miller's equilibrium for **fixed** $\frac{\Delta r}{\Delta \theta}$ and $\frac{\partial^2}{\partial \psi^2} \Phi_0(\psi)$.

Variation of mean ExB shearing rate with triangularity δ

- Maximum shear off the outboard mid-plane for for $\delta < \delta_{crit}$ (~NT) \rightarrow Shearing is less effective for $k_x = 0$ modes i.e, the modes ballooning at $\theta = 0$.
 - Shear at $\theta = 0$:
 - \$\psi\$ with increasing NT.
 - Weaker for NT than for PT. Note that fluctuations balloon at $\theta = 0$. Thus, shearing efficiency $\downarrow \Longrightarrow P_{L \to H, th} \uparrow (!?)$.

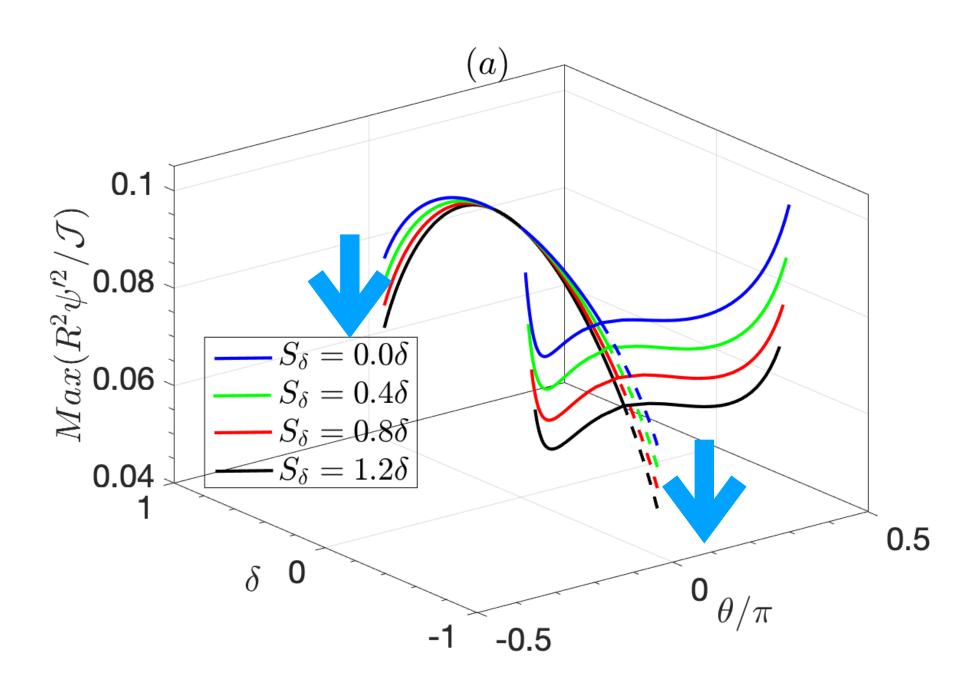


• Flux surface averaged shearing rate is higher for NT than for PT. -Global confinement ?!



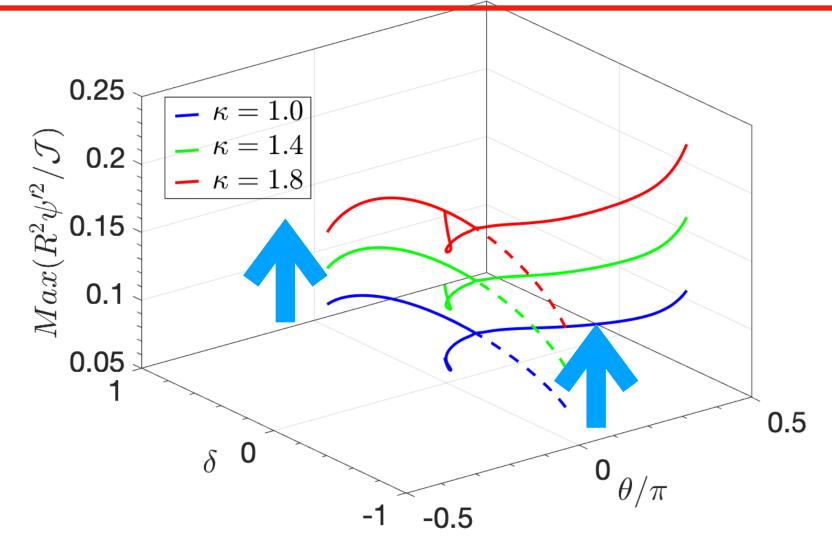
• Maximum shear above the outboard mid-plane for for $\delta_u < \delta_{u.crit} \& \delta_l > \delta_u$

ExB shearing rate variations with triangularity gradient S_{δ} , elongation κ and elongation gradient S_{κ}

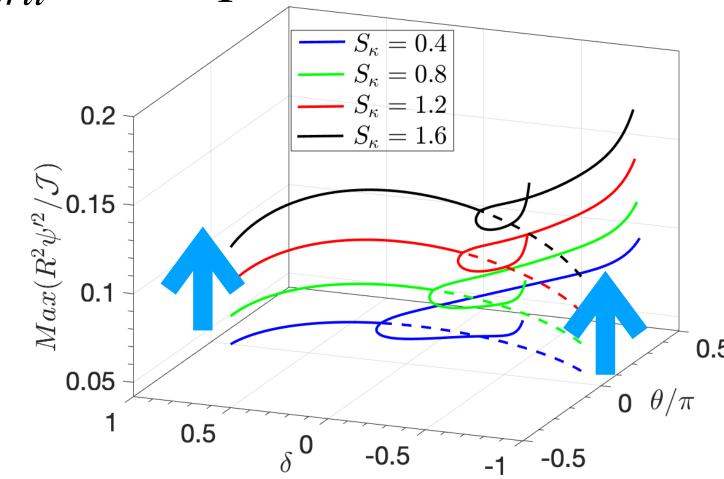


On increasing $|S_{\delta}|$:

- Shearing rate decreases.
- δ_{crit} moves toward δ^- .
- → Radial profile of triangularity matters!
- → Can triangularity profile can be tailored to boost mean ExB shear?



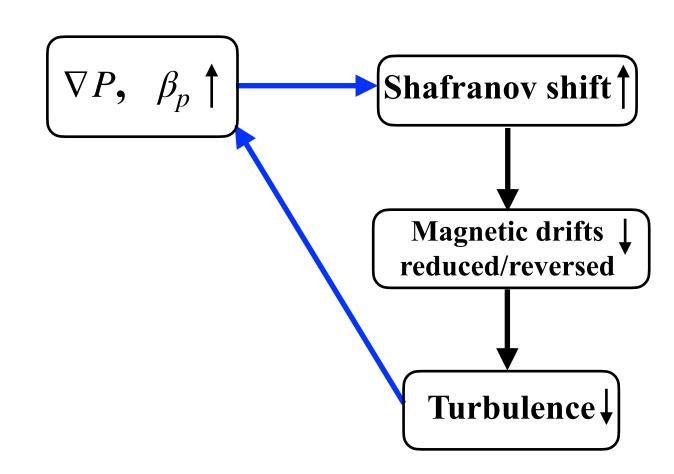
- Shearing rate increases with κ
- δ_{crit} is independent of κ .



- Shearing rate increases with S_k .
- δ_{crit} moves along δ^- .

Shafranov shift induced transport bifurcation

• ITB formation in high- β_p regime is often linked to transport bifurcation due to turbulence stabilization by Shafranov shift due to mag drift reduction/reversal, *ignoring* the mean ExB shear effect. [M Beer+PoP 1997, S Ding+PoP 2017, J McClenaghan+PoP 2019, G M Staebler+PoP 2017]



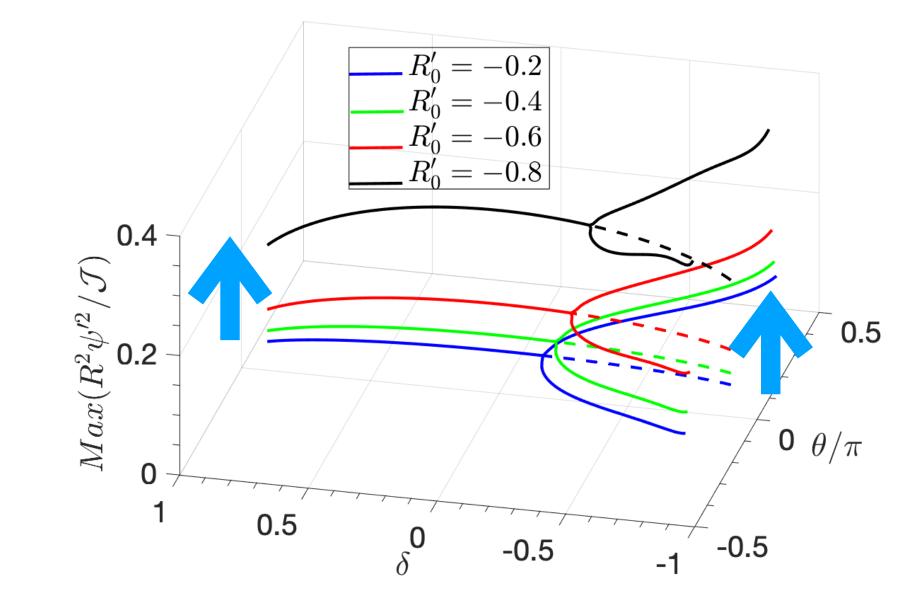
Feedback loop for Shafranov shift induced transport bifurcation

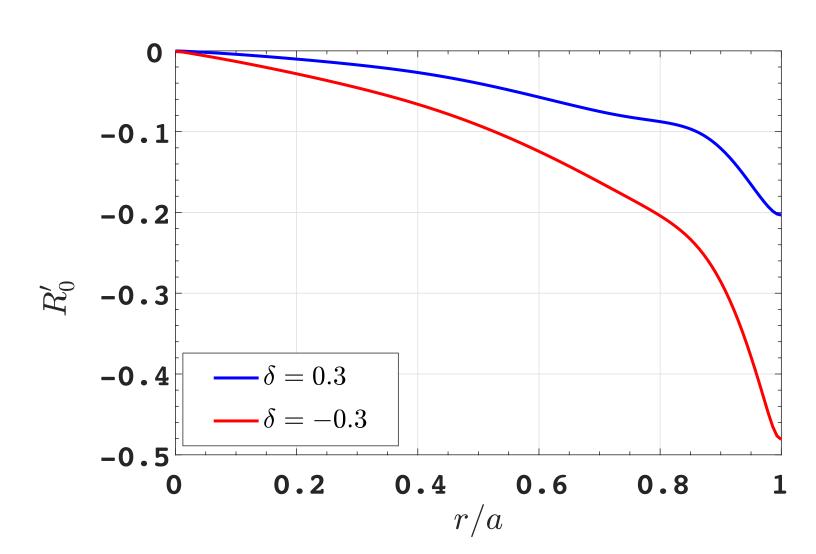
- But... like it or not mean shear *exist* in high- β_p discharges!
- So, how does mean shear and Shafranov shift interact?
- Interplay of mean ExB shear, Shafranov shift and NT?

Variation of mean ExB shearing rate with Shafranov shift gradient R'_0

On increasing $-R'_0$:

- Shearing rate increases for all δ .
- δ_c moves toward δ^- on increasing $-R_0'$.
- Key reason—flux compression.





Shafranov shift gradient obtained using CHEASE code

Significant for:

- high β_p regime (i.e, RS ITB) as $R_0' \propto \frac{r}{R_0} \beta_p$
- NT shapes
 - as $\beta_p(\delta^-) > \beta_p(\delta^+)$
 - Numerical MHD equilibrium study shows $R_0'(\delta^-) > R_0'(\delta^+)$ even for fixed β_p .
- → Even more significant for future NT+ITB discharges

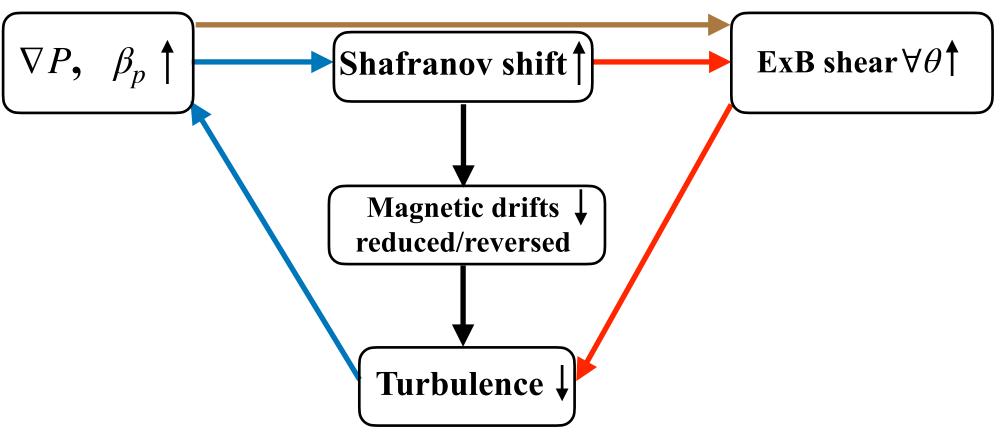
Implications of Shafranov shift effect on ExB shear

- Shafranov shift affects turbulence in 2 distinct ways:
 - (I) Stabilizes turbulence by reduction/reversal of magnetic drifts
 - (II) Directly enhances the mean shear, \rightarrow additional turbulence suppression

Bifurcation by (I) is often invoked as a mechanism of confinement improvement in high- β_p regime, ignoring the mean shear effect.

Mean ExB shear ↑ by Shafranov shift → +ve feedback on the feedback loop of the Shafranov shift induced transport bifurcation.

Shafranov shift has a +ve effect on the mean ExB shear induced transport bifurcation, through: (a) $\gamma_{lin} \downarrow$, and (b) ExB shear \uparrow .



Both (I) and (II) can work in tandem to reduce the ∇P_{crit} for the onset of ITB in reversed shear PT shape

Conclusions

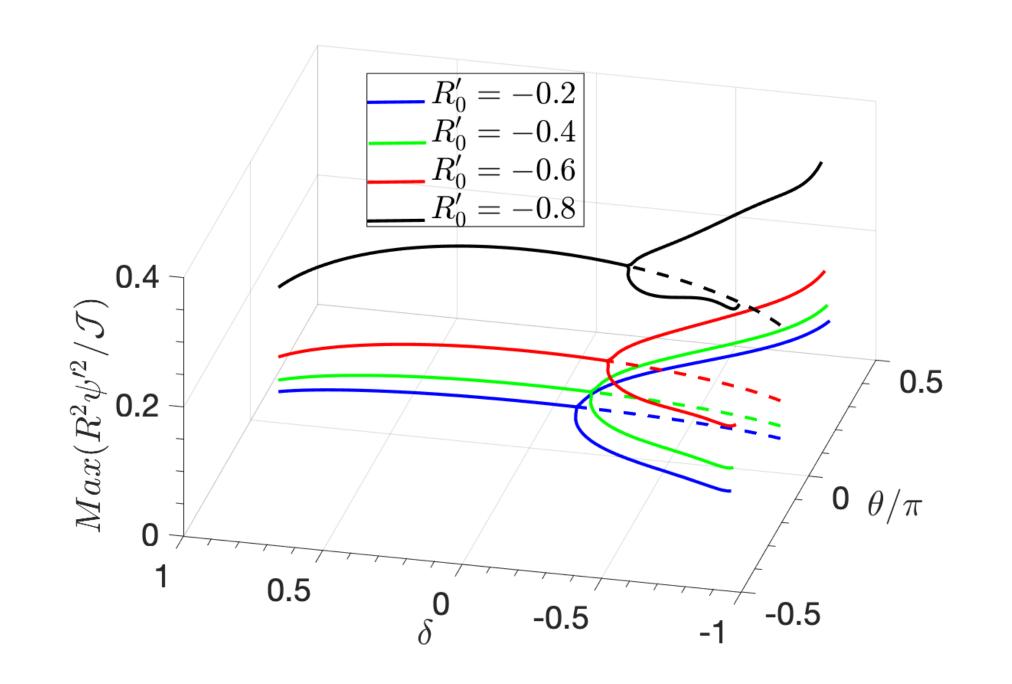
- Maximum shear off the outboard mid-plane for $\delta < \delta_{crit} (\leq 0)$
 - → <u>Up-down symmetry:</u> Max shear located symmetrically above and below the outboard midplane for $\delta_u = \delta_l = \delta < \delta_{crit}$
 - ⇒ <u>Up-down asymmetry:</u> Max shear located above the outboard mid-plane for $\delta_u < \delta_{crit}$ & $\delta_l > \delta_u$. Max shear located below the outboard mid-plane for $\delta_l < \delta_{crit}$ & $\delta_u > \delta_l$.
 - Shear at $\theta = 0$ decreases with increasing NT. Fluctuations balloon at $\theta = 0$. Thus, shearing efficiency $\downarrow \Longrightarrow P_{L \to H, th} \uparrow (!?)$. Is this sufficient?

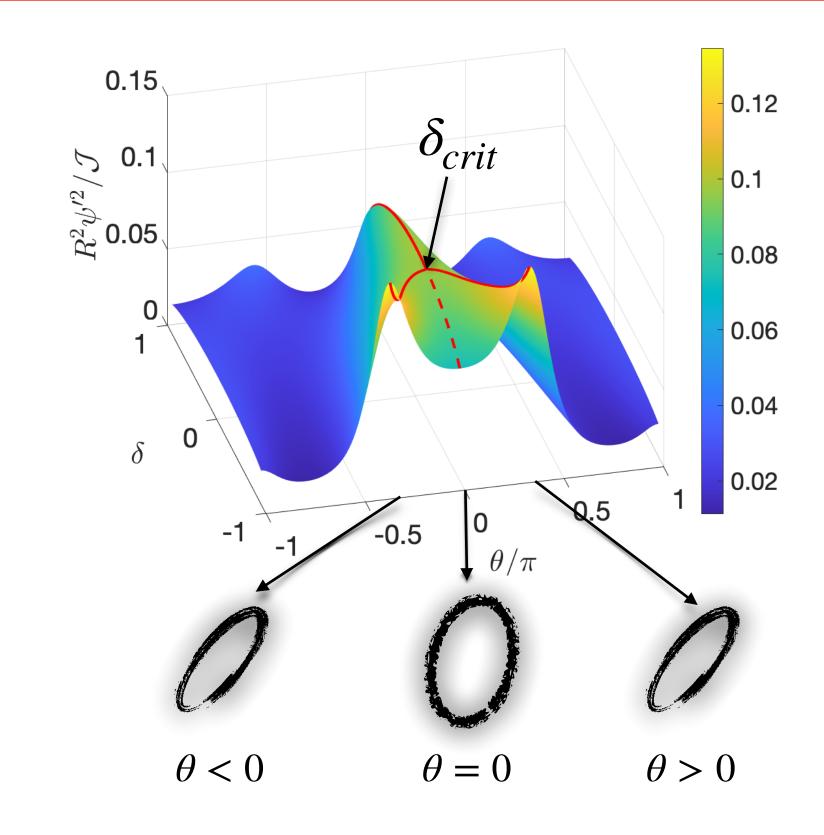
• Direct effect of Shafranov shift gradient $-R'_0$ on shearing rate: Shearing rate increases with increasing $-R'_0$ for all δ . Key reason \rightarrow flux compression. Significant for high β_p regime and NT shapes.

These results has implications not just for confinement & L-H transition for NT but also for ITB discharges in PT and NT(proposed), and NT core and and pedestal.

For the experimentalists

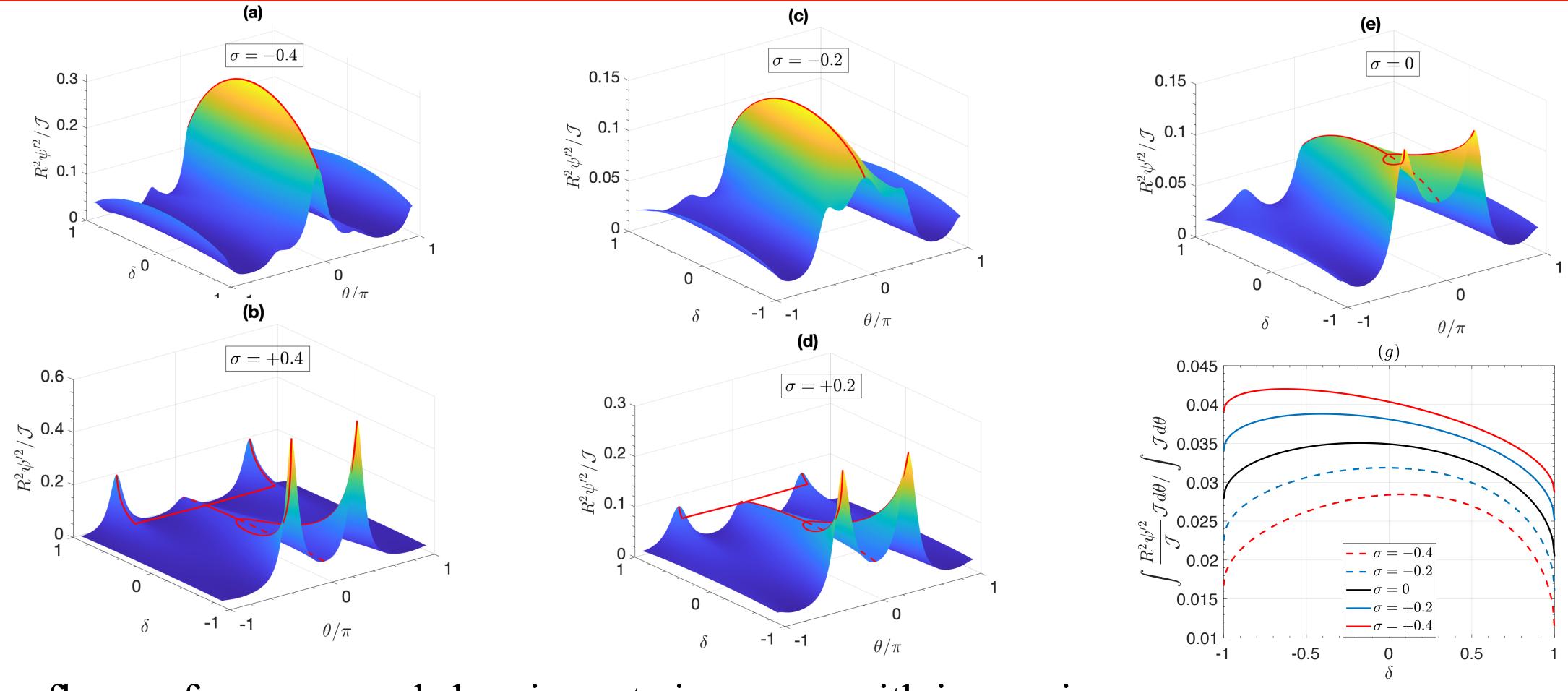
- Mean ExB Shearing is maximal off the mid-pane for NT: ⇒ Eddy tilting should be strongest off the mid-plane.
 - Direct imaging using gas-puffing.
 - Joint pdf of radial and poloidal velocity fluctuations (i.e., \tilde{v}_r & \tilde{v}_θ) should show max tilting (most-correlated) off the mid-plane for NT.
 - Up-down asymmetric tilting distribution for $\delta_u \neq \delta_l$





- Shafranov shift gradient R_0' directly boosts the mean ExB shear:
 - Re-assess the role of mean ExB shear in high- β_p reverse shear discharges.

Back-up: ExB shearing rate variations with squareness σ



- ullet The flux surface averaged shearing rate increases with increasing σ
- Shearing at $\theta = 0$ decreases with increasing σ .
- For σ < 0 the the geometric bifurcation disappears, the poloidal width of shear gets narrow and the shearing at θ = 0 increases.