

# **Physics of SOL Broadening by Turbulence**

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# Background

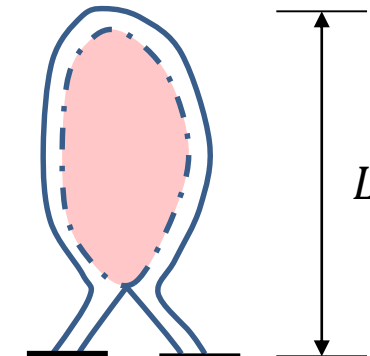
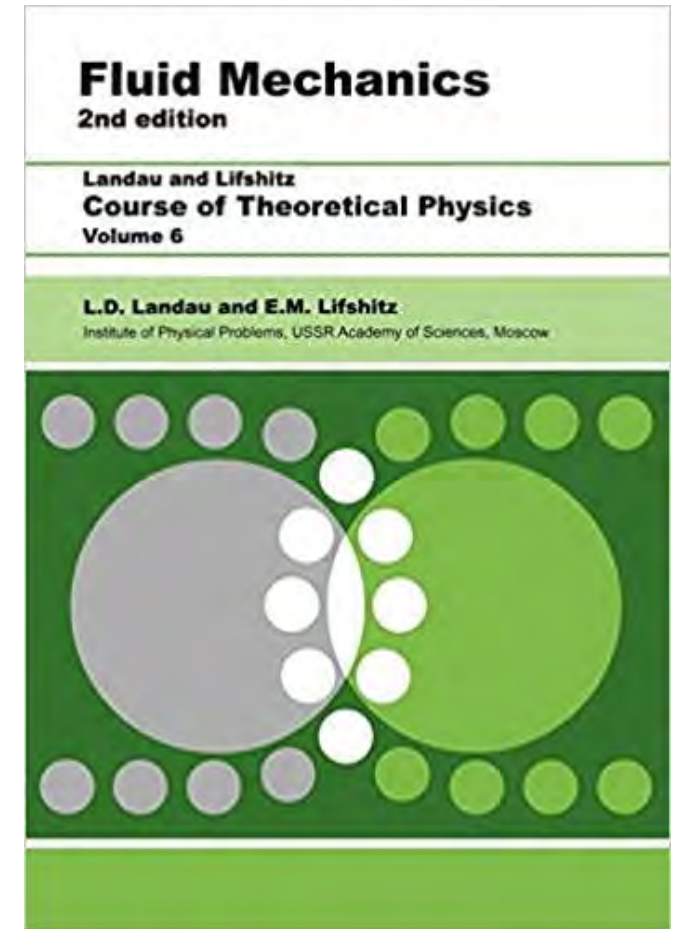
- Conventional Wisdom of SOL:

(cf: Stangeby...)

- Turbulent Boundary Layer, ala' Blasius, with  $D$  due turbulence
- $\delta \sim (D\tau)^{1/2}, \tau \approx L_c/V_{th}$
- $D \leftrightarrow$  local production by SOL instability process  
→ familiar approach,  $D$  ala' QL

- Features:

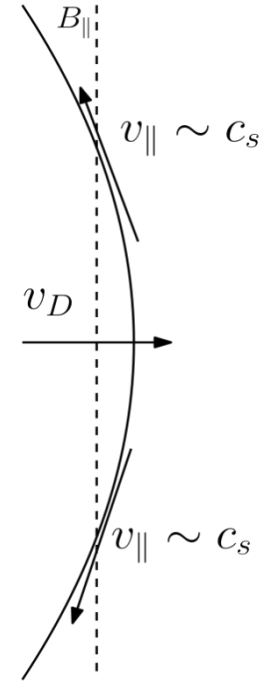
- Open magnetic lines → dwell time  $\tau$  limited by transit, conduction, ala' Blasius
- Intermittency → “Blobs” etc. Observed. **Physics?**



# Background, cont'd

- But... Heuristic Drift (HD) Model (Goldston +)

- $V \sim V_{\text{curv}}$  ,  $\tau \sim L_c/V_{\text{thi}}$  ,  $\lambda \sim \epsilon \rho_{\theta i}$  → SOL width
- Pathetically small
- Pessimistic  $B_\theta$  scaling, yet high  $I_p$  for confinement
- Fits lots of data.... (Brunner '18, Silvagni '20)



- Why does neoclassical work? → ExB shear suppresses SOL modes i.e.

$$\gamma_{\text{interchange}} \sim \frac{c_s}{(R_c \lambda)^{\frac{1}{2}}} - \frac{3T_{\text{edge}}}{|e|\lambda^2}$$

shearing  $\leftrightarrow$  strong  $\lambda^{-2}$  scaling

$$\text{from: } \frac{c_s}{(R_c \lambda)^{\frac{1}{2}}} - \langle V_E \rangle'$$

# Background, cont'd

- THE Existential Problem... (Kikuchi, Sonoma TTF):

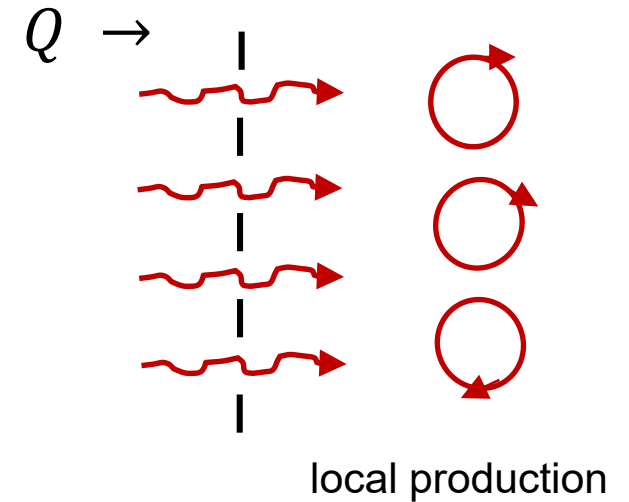
Desire  $\left\{ \begin{array}{l} \text{Confinement} \rightarrow \text{H-mode} \leftrightarrow \text{ExB shear} \\ \text{Power Handling} \rightarrow \text{broader heat load, etc} \end{array} \right. \rightarrow \text{Both to be good !}$

How reconcile? – Pay for power mgmt with confinement ?!

- Spurred:
  - Exploration of turbulent boundary states with improved confinement: Grassy ELM, WPQHM, I-mode, Neg. D ... N.B. What of ITB + L-mode edge?
  - + SOL width now key part of the story
  - Simulations, Visualizations (XGC, BOUT...) ~ “Go” to ITER and all be well
- But... What’s the Physics ?? How is the SOL broadened?

# SOL BL Problem

- SOL Excitation
  - Local production (SOL instabilities)
  - Turbulence energy influx from pedestal
- Key Questions:
  - Local drive vs spreading ratio  $\rightarrow Ra$
  - Is the SOL usually dominated by turbulence spreading?
  - How far can entrainment penetrate a stable SOL  $\rightarrow$  SOL broadening?
  - Effects ExB shear, role structures ?



# Physics Issues – Part II

- How calculate SOL width for turbulent pedestal but a locally stable SOL?

- spreading penetration depth

- must recover HD in WTT limit

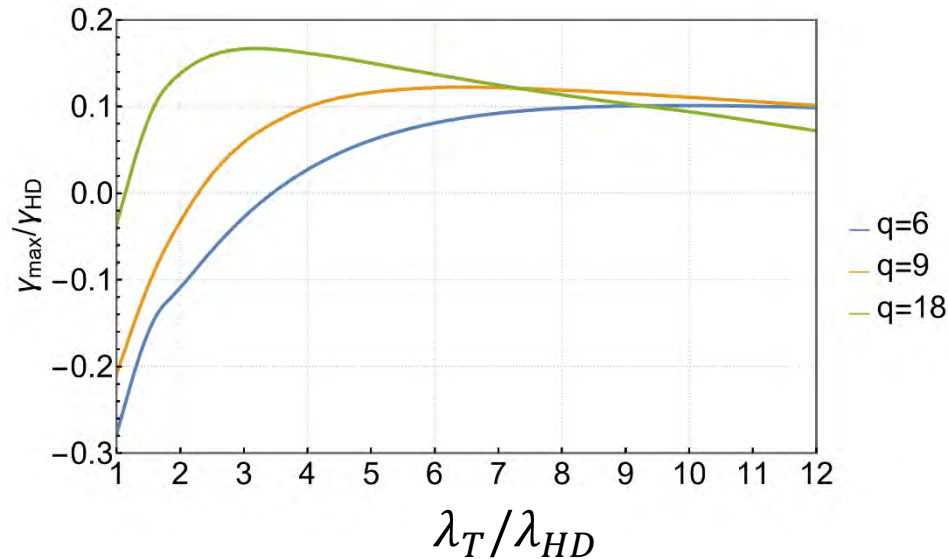
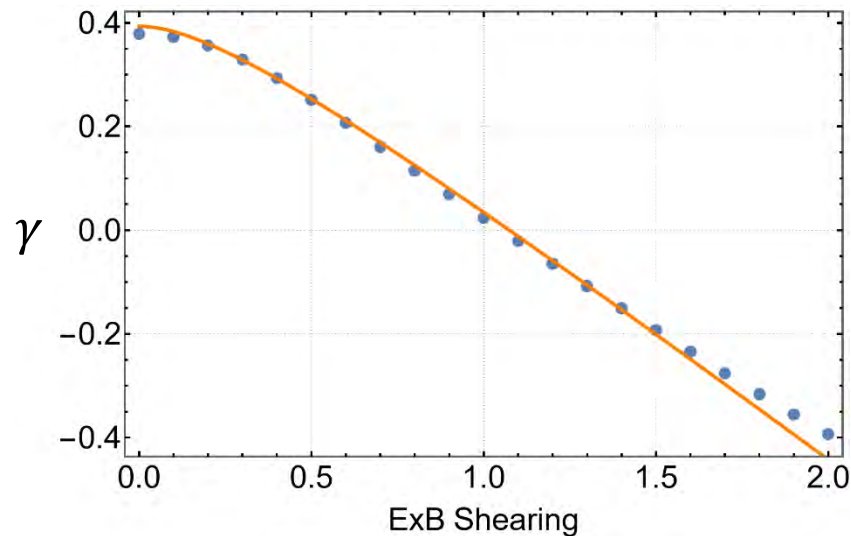
➔ • Scaling and cross-over of  $\lambda_q$  relative HD model

➔ • What is effect/impact of barrier on spreading mechanism?

- Can SOL broadening and good confinement be reconciled ?

# Model 1 – Stable SOL – Linear Theory

- Standard drift-interchange with sheath boundary conditions + ExB shear (after Myra + Krash.)



Maximal Linear Growth Rate of Interchange Mode in the SOL v.s. normalized layer width  $\lambda_D/\lambda_{HD}$  at different SOL safety factor  $q$  (with  $\beta = 0.001$ )

Linear Growth Rate of a specific mode (fixed  $k_y$ ) v.s.  $E \times B$  shear at  $q = 5, \beta = 0.001, k_y \cdot \lambda_{HD} = 1.58$ .

- Relevant H-mode ExB shear strongly stabilizing  $\gamma_{HD} = c_s/(\lambda_{HD}R)^{1/2}$
- Need  $\lambda/\lambda_{HD}$  well above unity for SOL instability.  $V'_E \approx \frac{3T_e}{|e|\lambda^2} \rightarrow$  layer width sets shear

# Model 2 – Two Multiple Adjacent Regions

- “Box Model” – after Z.B. Guo, P.D.

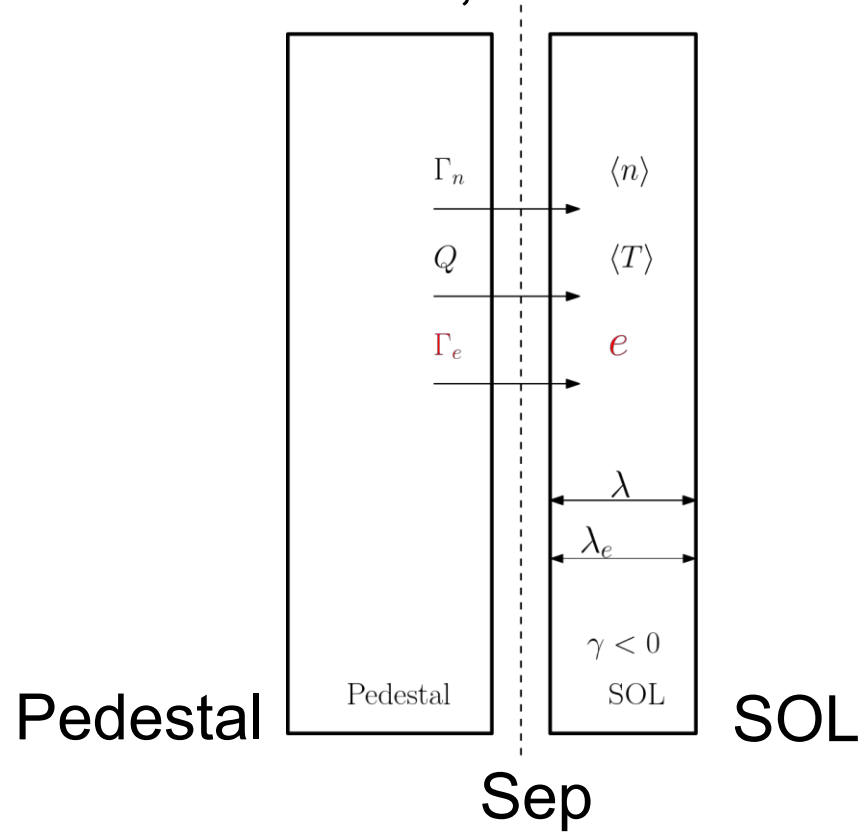


Illustration of Two Box Model: SOL driven by particle flux, heat flux and intensity flux ( $\Gamma_e$ ) from the pedestal. The horizontal axis is the radial direction, and vertical axis is the poloidal direction.

- Key Point:
  - Spreading flux from pedestal can enter stable SOL
  - Depth of penetration → extent of SOL broadening
  - Problem in one of entrainment/penetration



# Width of Stable SOL

- Fluid particle:  $\frac{dr}{dt} = V_{Dr} + \tilde{V}$ 
  - $V_{Dr}$ : drift
  - $\tilde{V}$ : fluctuating velocity
- Dwell time:  $\tau_{\parallel}$

{ Dwell time  $\tau_{\parallel}$   
constrains excursion

- $\delta^2 = \langle (\int (V_D + \tilde{V}) dt) (\int (V_D + \tilde{V}) dt) \rangle$

$\langle (\text{step})^2 \rangle = V_D^2 \tau_{\parallel}^2 + \langle \tilde{V}^2 \rangle \tau_c \tau_{\parallel}$

correlation time  
modest turbulence  $\leftrightarrow \tau_c \geq \tau_{\parallel}$

$= \lambda_{HD}^2 + \varepsilon \tau_{\parallel}^2$

turbulence energy density

{ See also  
Fokker-Planck analysis  
i.e. drift + diffusion

- So  $\lambda = [\lambda_{HD}^2 + \varepsilon \tau_{\parallel}^2]^{1/2} \rightarrow$  SOL width [Effects add in quadrature]

- How compute  $\varepsilon$ ?  $\rightarrow$  turbulence energy !

# Calculating the SOL Turbulence Energy 1

- $K - \epsilon$  type model, mean field approach (c.f. Gurcan, P.D. '05 et seq)
  - Can treat various NL processes via  $\sigma, \kappa$
  - Exploit conservative form model
- $\partial_t \epsilon = \gamma \epsilon - \sigma \epsilon^{1+\kappa} - \partial_x \Gamma_e \quad \rightarrow \text{Spreading, turbulence energy flux}$ 
  - $\swarrow$  Growth  $\gamma < 0$   
here contains shear + sheath
  - $\searrow$  NL transfer  $\gamma_{NL} \sim \sigma \epsilon^\kappa$
- N.B.: No Fickian model of  $\Gamma_e$  employed
- Readily extended to 2D, improved production model, etc.

# Calculating the SOL Turbulence Energy 2

- Integrate  $\varepsilon$  equation  $\int_0^\lambda$
- Take quantities = layer average
- $\Gamma_{e,0} + \lambda_e \gamma \varepsilon = \lambda_e \sigma \varepsilon^{1+\kappa}$

Separatrix fluctuation energy flux

Single parameter characterizing spreading

So for  $\gamma < 0$ ,

$$\Gamma_{e,0} = \lambda_e |\gamma| \varepsilon + \sigma \lambda_e \varepsilon^{1+\kappa}$$

$\lambda_e$  = layer width for  $\varepsilon$

$\Gamma_{e,0}$  vs linear + nonlinear damping

# Calculating the SOL Turbulence Energy 3

[Mean Field Theory]

- Full system:

$$\Gamma_{e,0} = \lambda_e |\gamma| \varepsilon + \sigma \lambda_e \varepsilon^{1+\kappa}$$

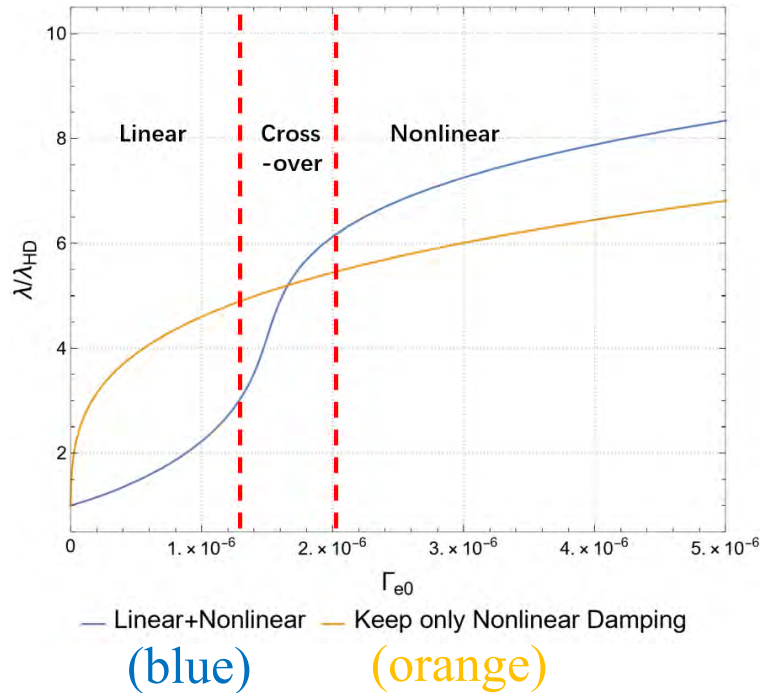
$$\lambda_e = [\lambda_{HD}^2 + \varepsilon \tau_{\parallel}^2]^{1/2}$$

Simple model of  
turbulent SOL  
broadening

- $\Gamma_{0,e}$  is single control parameter characterizing spreading
- $\tilde{\Gamma}_{0,e}$  ? Expect  $\tilde{\Gamma}_e \sim \Gamma_0$

# SOL width Broadening vs $\Gamma_{e,0}$

- SOL width broadens due spreading



$\lambda/\lambda_{HD}$  plotted against the intensity flux  $\Gamma_{e0}$  from the pedestal at  $q = 4, \beta = 0.001, \kappa = 0.5, \sigma = 0.6$

Variation indicates need for detailed scaling analysis

- Clear decomposition into
  - Weak broadening regime  $\rightarrow$  shear dominated
  - Cross-over regime
  - Strong broadening regime
- $\rightarrow$  NL damping vs spreading } relevant

- Cross-over for:
  - $\langle \tilde{V}^2 \rangle \sim V_D^2 \rightarrow$  cross-over  $\Gamma_{0,e}$
- Cross-over for  $\tilde{V} \sim O(\epsilon)V_*$

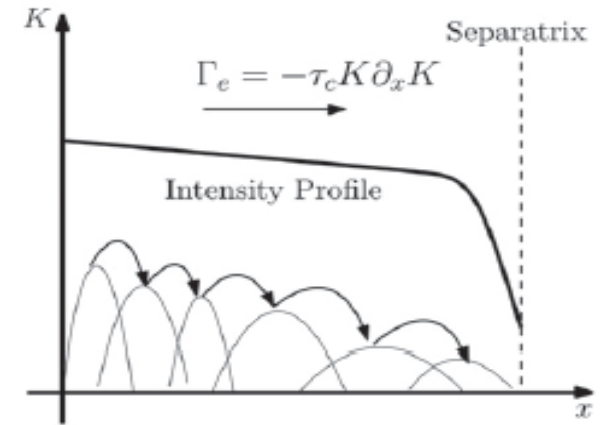
# Computing the Turbulence Energy Flux 1

- Need consider pedestal to actually compute  $\Gamma_{e,0}$

- Two elements

Does another trade-off loom? -- Pedestal Turbulence: Drift wave? Ballooning?

-- Effect of transport barrier  $\leftrightarrow$  ExB shear layer  $\rightarrow$  barrier permeability!?



- Key Point: shearing limits correlation in turbulent energy flux

$$\text{i.e. } \Gamma_{e,0} \approx -\tau_c I \partial_x I \approx \tau_c I^2 / w_{\text{ped}} \quad (\text{Hahm, PD +})$$

ped turbulence  
intensity

correlation time  $\rightarrow$  strongly sensitive to shearing

N.B. Caveat Emptor re: intensity flux closure !

# Computing the Turbulence Energy Flux 2

- Familiar analysis for  $D \rightarrow$  Kubo

$$D = \int_0^\infty d\tau \langle V(0)V(\tau) \rangle = \int_0^\infty d\tau \sum_k |\tilde{V}_k|^2 \exp[-k_y^2 \omega_s^2 D \tau^3 - k^2 D \tau]$$

- Strong shear (relevant)

$$\tau_c = \tau_t^{1/2} \omega_s^{-1/2}$$

$$\tau_t \sim 1 / k \tilde{V}, \quad \omega_s \sim V_E'$$

Here, via RFB  $\rightarrow \omega_s = \partial_r \frac{\nabla P_i}{n|e|} \sim \frac{\rho^2}{w_{ped}^2} \Omega_{ci}$

- $\tau_c + w_{ped} +$  turbulence intensity in pedestal gives  $\Gamma_{e,0} \approx \tau_c I^2 / w_{ped}$
- Need  $\Gamma_{e,0} \geq \Gamma_{e,\min} \approx |\gamma| \lambda_{HD}^3 \tau_{\parallel}^{-2}$

# Computing the Turbulence Energy Flux 3

- Pedestal → Drift wave Turbulence
- Necessary turbulence level:

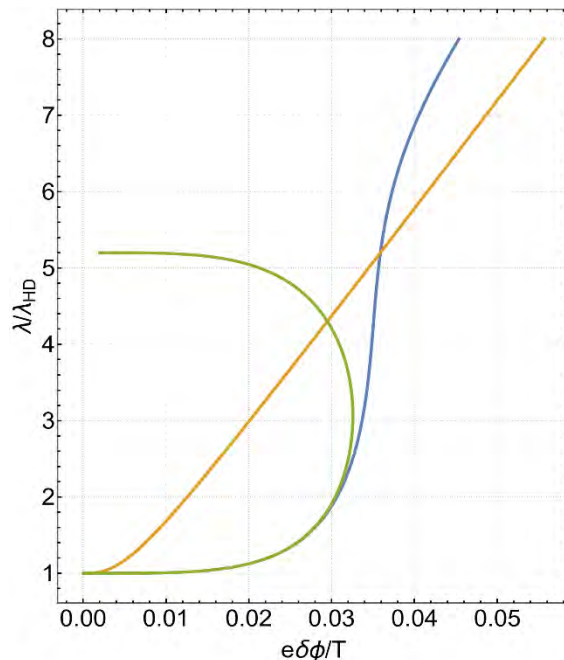
- Weak Shear  $\frac{\delta V}{c_s} \sim \left(\frac{\rho}{R}\right)^{1/2} q^{-1/4}$

- Strong Shear  $\frac{\delta V}{c_s} \sim \left(\frac{\rho}{R}\right)^{1/2} q^{-1/4} \left(\frac{w_{ped}}{\rho}\right)^{-1/8}$

blue – all damping

orange – nonlinear only

green – linear only



→  $\lambda/\lambda_{HD}$  vs  $|e|\hat{\phi}/T_e$  in pedestal

→  $\rho/R$  is key parameter

→ Broadens layer at acceptable fluctuation level

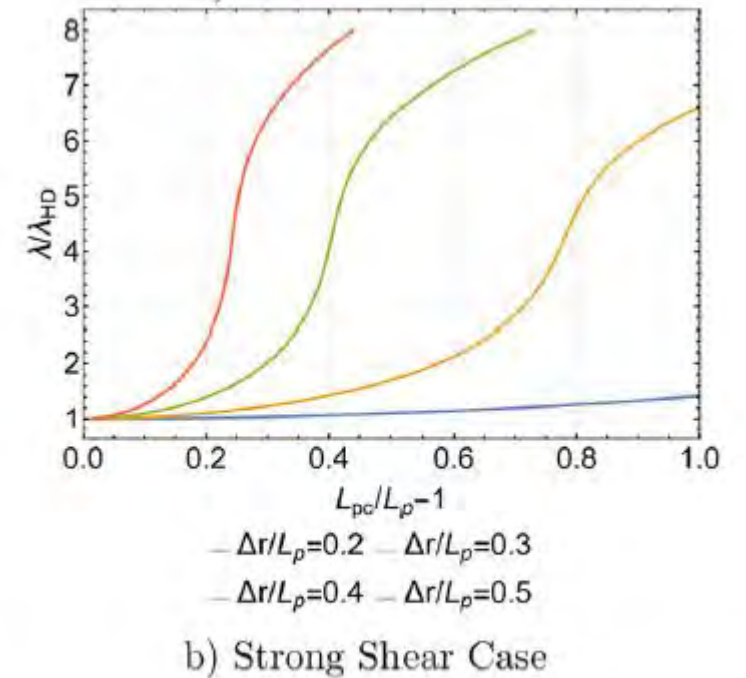


# Computing the Turbulence Energy Flux 4

- Pedestal  $\rightarrow$  Ballooning modes  $\rightarrow$  Grassy ELMs
- Necessary relate turbulence to  $L_{P,crit} / L_P - 1$
- Strong shear:

$$\frac{L_{Pc}}{L_P} - 1 \sim \left(\frac{q\rho}{R}\right)^{\frac{10}{7}} \left(\frac{R}{w_{ped}}\right)^{\frac{16}{7}} \left(\frac{w_{ped}}{\Delta_r}\right)^{\frac{16}{7}} \beta$$

- Supercriticality scales with  $\frac{\rho}{R}$ ,  $\beta_t$



**Figure 10.** Typical cases for ballooning. The normalized pedestal width  $\lambda/\lambda_{HD}$  is plotted against supercriticality  $L_{pc}/L_p - 1$  at different mode width  $\Delta/L_p$ .

# Computing the Turbulence Energy Flux 5 → Bottom Line

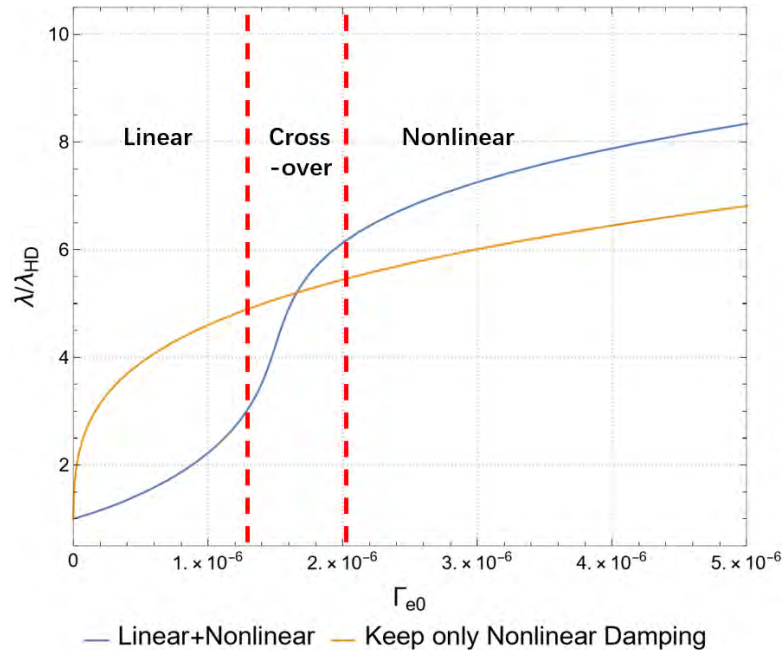
- SOL broadening to  $\lambda > \lambda_{HD}$  achievable at tolerable pedestal fluctuation levels
- DW levels scale  $\sim \left(\frac{\rho}{R}\right)^{1/2}$
- Ballooning supercritical scale  $\sim \left(\frac{\rho}{R}\right)^{10/7} \beta$
- ‘Grassy ELM’ state promising
- Sensitivity analysis → Cross over  $\varepsilon$  determined primarily by linear damping (shear). Conclusion  $\sim$  insensitive to NL saturation

# Partial Summary

- Turbulent scattering broadens stable SOL

$$\lambda = (\lambda_{HD}^2 + \varepsilon \tau_{\parallel}^2)^{1/2}$$

- Separatrix turbulence energy flux specifies SOL turbulence drive



$$\Gamma_{0,e} = \lambda_e |\gamma| \varepsilon + \lambda \sigma \varepsilon^{1+\kappa}$$

Broadening increases with  $\Gamma_{0,e}$   
cross-over for  $\langle \tilde{V}^2 \rangle \sim V_D^2$

Non-trivial dependence

- $\Gamma_{0,e}$  must overcome shear layer barrier

Yes – can broaden SOL to  $\lambda/\lambda_{MHD} > 1$  at tolerable fluctuation levels

Further analysis needed

# Broader Messages

- Turbulence spreading is important – even dominant – process in setting SOL width.  $\Gamma_{0,e}$  is critical element.  $\lambda = \lambda(\Gamma_{0,e}, \text{parameters})$
- Production Ratio  $R_a$  merits study and characterization
- ➔ • Spreading is important saturation mechanism for pedestal turbulence
- Simulation should stress calculation and characterization of turbulence energy flux over visualizations and front propagation studies.
- Critical questions include local vs FS avg, channels and barrier interaction, Turbulence ‘Avalanches’
- ➔ • Turbulent pedestal states attractive for head load management

# Open Issues

- Quantify  $\lambda = \lambda \left( \frac{|e|\hat{\phi}|}{T} \Big|_{ped} \right)$  dependence



- Structure of Flux-Gradient relation for turbulence energy?
- Phase relation physics for intensity flux? – crucial to ExB shear effects
- Kinetics  $\rightarrow \langle \tilde{V}_r \delta f \delta f \rangle$ , Local vs Flux-Surface Average, EM
- SOL Diffusive?  $\rightarrow$  Intermittency('Blob'), Dwell Time ?
- SOL  $\rightarrow$  Pedestal Spreading ?  $\leftrightarrow$  HDL (Goldston) ?  
i.e. Tail wags Dog ? Both wagging ?  $\rightarrow$  Basic simulation, experiment ?  
Counter-propagating pulses ?